

AD 391: Lateral Torsional Buckling of rectangular plates in accordance with BS EN 1993-1-1

BS EN 1993-1-1 does not explicitly cover LTB of rectangular plates. This AD note provides guidance for calculating the design buckling resistance moment ($M_{b,Rd}$) that can be used for BS EN 1993-1-1. To calculate $M_{b,Rd}$ it is necessary to determine the non-dimensional slenderness $\bar{\lambda}_{LT}$. This AD note gives two methods of calculating $\bar{\lambda}_{LT}$ for a plate. The first method is from first principles, using the formula for the elastic critical moment M_{cr} of a plate; the second is by using the formula for the equivalent slenderness λ_{LT} of a plate given in Appendix B, clause B.2.7 of BS 5950-1.

For BS 5950-1, AD note 310 (Staircases with flat stringers) discusses the design of steel stairs with flat plate stringers. It suggests the design of the stringers can be carried out by determining the buckling resistance of the stringer over a buckling length equal to the tread spacing, assuming the stringer is class 3.

Method 1 to determine $\bar{\lambda}_{LT}$:

Starting from first principles, the non-dimensional slenderness of a plate can be determined as follows:

The standard moment for the elastic critical moment of an I section is:

$$M_{cr} = C_1 \frac{\pi^2 E I_z}{l^2} \sqrt{\frac{I_w}{I_z} + \frac{I^2 G I_T}{\pi^2 E I_z}}$$

Under uniform moment, $C_1 = 1.0$. For a plate, there is no term involving the warping constant I_w because the section has no flanges and it is assumed axial stresses due to warping are not developed. The formula for a plate therefore reduces to:

$$M_{cr} = \frac{\pi}{l} \sqrt{E I_z G I_T}$$

Making the substitutions $I_z = \frac{dt^3}{12}$, $I_T = \frac{dt^3}{3}$ and $G = \frac{E}{2(1+\nu)}$

where ν is Poisson's ratio and equals 0.3 for steel.
 t and d are the thickness and depth of the plate respectively.

$$\text{Therefore } M_{cr} = \frac{dt^3}{6} \frac{\pi E}{l} \sqrt{\frac{1}{2.6}} \quad (\text{Equation 1})$$

Assuming a class 3 cross-section, the non-dimensional slenderness is given in BS EN 1993-1-1 (clause 6.3.2.2 (1)) by the formula:

$$\bar{\lambda}_{LT} = \sqrt{\frac{W_{el} f_y}{M_{cr}}} \quad (\text{Equation 2})$$

where $W_{el} = d^2 t / 6$

Method 2 to determine $\bar{\lambda}_{LT}$:

Substituting for M_{cr} from equation 1 and $W_{el} = d^2 t / 6$ into equation 2, leads to:

$$\bar{\lambda}_{LT} = \sqrt{\frac{f_y \times 1.0 \times \sqrt{2.6} \, ld}{\pi E} \frac{1}{t^2}} = \sqrt{\frac{f_y}{\pi^2 E} \frac{1.0 \pi \times \sqrt{2.6} \, ld}{1} \frac{1}{t^2}} \approx \sqrt{\frac{f_y}{\pi^2 E}} \times 2.8 \sqrt{\frac{0.667 ld}{t^2}}$$

The quantity $\sqrt{\frac{\pi^2 E}{f_y}}$ is denoted λ_1 in BS EN 1993-1-1 and is the slenderness

at which the Euler load equals the squash load.

Starting from the formula in BS 5950-1, clause B.2.7 the equivalent slenderness is given as:

$$\lambda_{LT} = 2.8 \sqrt{\frac{\beta_w ld}{t^2}} \quad (\text{Equation 3})$$

For a class 3 section, $\beta_w = 2/3 = 0.667$.

Therefore for design to BS EN 1993-1-1, the non-dimensional slenderness $\bar{\lambda}_{LT}$ of a plate can be stated as:

$$\bar{\lambda}_{LT} = \frac{\lambda_{LT}}{\lambda_1} \quad (\text{Equation 4})$$

For $f_y = 275$, $\lambda_1 = \pi \times \sqrt{\frac{210000}{275}} = 87$

for $f_y = 355$, $\lambda_1 = 76$

The design buckling resistance $M_{b,Rd}$ can then be calculated from clause 6.3.2.1 (3) (equation 6.55) assuming a class 3 cross-section. The reduction factor χ_{LT} is calculated from clause 6.3.2.2 (1) (equation 6.56) based on curve d (i.e imperfection factor $\alpha_{LT} = 0.76$)

The non-dimensional slenderness $\bar{\lambda}_{LT}$ may be determined from equation 2 or 4 above.

Contact: **Richard Henderson**

Tel: **01344 636525**

Email: **advisory@steel-sci.com**

New and revised codes & standards

From BSI Update September 2015

BS EN PUBLICATIONS

BS EN 10338:2015

Hot rolled and cold rolled non-coated products of multiphase steels for cold forming. Technical delivery conditions
No current standard is superseded.

BS EN 10346:2015

Continuously hot-dip coated steel flat products for cold forming. Technical delivery conditions
Supersedes BS EN 10346:2009

BRITISH STANDARDS UNDER REVIEW

BS ISO 4992-1:2006

Steel castings. Ultrasonic examination. Steel castings for general purposes.

BS ISO 4992-2:2006

Steel castings. Ultrasonic examination. Steel castings for highly stressed components

NEW WORK STARTED

BS 7668

Weldable structural steels. Hot finished structural hollow sections in weather resistant steels. Specification
Will supersede BS 7668:2004

EN ISO 17660-1

Welding. Welding of reinforcing steel. Load-bearing welded joints
Will supersede BS EN ISO 17660-1:2006

EN ISO 17660-2

Welding. Welding of reinforcing steel. Non load-bearing welded joints.
Will supersede BS EN ISO 17660-2:2006

NA to EN 1993-1-4

UK National Annex to Eurocode 3. Design of steel structures. General rules. Supplementary rules for stainless steels.